



Extended-MHD simulations of disruption mitigation in SPARC using massive gas injection*

Andreas Kleiner¹

N.M. Ferraro¹, B. Lyons², M. Reinke³, R. Sweeney^{4,3}

¹Princeton Plasma Physics Laboratory ²

²General Atomics

³Commonwealth Fusion Systems ⁴Massachusetts Institute of Technology

*Work supported by Commonwealth Fusion Systems and by the US Department of Energy under contract DE-AC0204CH11466. This work was funded under the INFUSE program - a DOE SC FES private-public partnership.



e Physical model & simulation setup

6 Preliminary Results

4 Summary & Outlook

- SPARC follows high field path to fusion energy using HTS magnets
- D-T fusion
- ▶ First plasma planned for 2025

Some device parameters:

$$B_T = 12.2 \text{ T}$$

 $I_p = 8.7 \text{ MA}$
 $R_0 = 1.85 \text{ m}$
 $a = 0.57 \text{ m}$



[T. Henderson, CFS/MIT-PSFC]





- ► SPARC will use massive gas injection (MGI) for disruption mitigation
- > Injection of impurities can mitigate disruptions by radiating parts of the stored energy
- How do MGI parameters (injection rate, location & number of injectors) affect heat loads, thermal quench (TQ) time, toroidal peaking factor, wall forces, etc.?



e Physical model & simulation setup

Preliminary Results

Outlook

Modeling massive gas injection in SPARC with M3D-C1



5/16

- M3D-C1 uses integrated model
 - Extended-MHD for mascroscopic evolution of disruption dynamics
 - KPRAD [Whyte et al. (1997)] models ionization, recombination and radiation
- Spatially resolved conducting elements inside wall modeled with realistic resistivities
 Note: Passive plates were removed from SPARC design
- Anisotropic resistivity to represent ports











- Non-linear extended-MHD initial value stability code [Jardin et al., Comput. Sci. Discov. 5 014002, 2012]
 [Ferraro et al., Phys. Plasmas 23 056114, 2016]
- C^1 (quintic) finite element mesh
- Extended-MHD region beyond LCFS, resistive wall, vacuum region
- Single-fluid model, Spitzer resistivity ($S \sim 10^9$)

 $\frac{\partial n}{\partial t} + \nabla \cdot (n\vec{u}) = \Sigma \qquad \text{with } \Sigma := \sigma + D\nabla^2 n$ $nm_i \left(\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u}\right) = \vec{J} \times \vec{B} - \nabla p - \nabla \cdot \Pi + \vec{F} - m\vec{v}\Sigma$ $\frac{\partial p}{\partial t} + \vec{u} \cdot \nabla p + \Gamma p \nabla \cdot \vec{u} = (\Gamma - 1) \left[Q - \nabla \cdot \vec{q} + \eta J^2 - \vec{u} \cdot \vec{F} - \Pi : \nabla u - \frac{1}{2}mv^2\Sigma \right]$

 $ec{E} = -ec{u} imes ec{B} + \eta ec{J}$, $ec{J} = rac{1}{\mu_0}
abla imes ec{B}$, $rac{\partial ec{B}}{\partial t} = -
abla imes ec{E}$



- Coronal equilibrium not assumed
- Ionization and recombination determine impurity charge state evolution
- ▶ Radiation rates L_k taken from ADPAK database $(P_{rad,k} = n_k n_e L_k)$
- Impurity (Ne) is injected at zero temperature and brought to T_i upon ionization
- Loss of thermal energy due to ionization, line radiation, bremsstrahlung, recombination radiation
- Subcycling much faster than MHD time step

[Whyte et al., Proc. of 24th European Conference on Controlled Fusion and Plasma Physics, vol. **21A**, p. 1137, 1997] [Ferraro et al, Nucl. Fusion **59** 016001, 2019]



SPARC MGI simulation setup

- Up to 6 different injectors
 - Up-down symmetric: 6, 4, 2
 - Asymmetric: 5, 1
- Injected gas is mixture of neutral Ne and ionized D (1:10 ratio) with Gaussian shape and toroidally localized
- ► Total injection rate: 7.5×10²³ Ne/s for 6 injectors
 - Rate per injector is held constant
 - Number of injected particles scales with number of injectors







Physical model & simulation setup

6 Preliminary Results

Outlook



Shown here: 6 injector case

- MGI triggers low-n edge modes
- SPARC baseline case exhibits sawtooth, but no core radiation in early phase
- This is followed by stochastization of core







• Impurity is injected at t = 0



- ▶ Thermal energy W_{th} decreases due to radiation and conduction (sensitive to κ and D)
- ▶ In pre-TQ Loss of W_{th} scales with number of injectors
- With 1 injector TQ happens earlier than in 6 injector case
- Spikes of radiation occur in all cases during pre-TQ phase
- Simulations still in progress

Andreas Kleiner



Shown here: 6 injector case





Shown here: 2 injector case





Simulations use different widths for impurity Gaussian

# Injectors	Injector width	Total rate of injection	TPF max
1	0.08	$1.25 imes10^{23}$	12.6
2	0.08	$2.50 imes10^{23}$	14.2
4	0.08	$5.00 imes10^{23}$	≈ 8
5	0.24	$6.25 imes10^{23}$	4.9
6	0.24	$7.50 imes10^{23}$	≈ 3
2	0.8	$7.50 imes10^{23}$	5.5

- ▶ Width of gas plumes directly affects TPF as a result of localized impurities
- TPF is not correlated with low-n MHD activity
- Distributing injector sites toroidally reduces TPF



- Simulations use different widths for impurity Gaussian
- ▶ Total injection rate: 7.5×10²³ Ne/s



- TQ is slightly delayed in 6 injector case
- End of TQ: Energy from Ohmic heating converted to radiation



- Simulations use different widths for impurity Gaussian
- ▶ Total injection rate: 7.5×10²³ Ne/s



- ▶ 6 injectors result in slightly lower current peak
- No significant vertical displacement until at least early CQ



2 Physical model & simulation setup

Preliminary Results

Outlook & Outlook

- Recent improvements to the M3D-C1 model allow higher-fidelity disruption simulations
- Early onset of sawtooth and edge instabilities
- Thermal quench happens earlier with fewer injectors
- Radiation stays localized in pre-TQ phase and during TQ
- Decrease of thermal energy due to thermal conduction and radiated power
- ▶ TPF does not correlate well with low-*n* MHD activity
 - Spreading gas injectors toroidally, i.e. using 6 injectors helps decrease radiation PF
- Impurities are advected by bulk plasma flow only (no local increase in pressure or equilibrium flow)
 - Localization of impurities / radiation could be reduced by adding toroidal flows and with multi-fluid model







 Non-linear extended-MHD initial value stability code [Jardin et al., Comput. Sci. Discov. 5 014002, 2012]

$$\begin{aligned} \frac{\partial n}{\partial t} + \nabla \cdot (n\vec{u}) &= 0 \\ nm_i \left(\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} \right) &= \vec{J} \times \vec{B} - \nabla p - \nabla \cdot \Pi + \vec{F} \\ \frac{\partial p}{\partial t} + \vec{u} \cdot \nabla p + \Gamma p \nabla \cdot \vec{u} &= (\Gamma - 1) \left[Q - \nabla \cdot \vec{q} + \eta J^2 - \vec{u} \cdot \vec{F} - \Pi : \nabla u \right] \\ &+ \frac{1}{ne} \vec{J} \cdot \left(\frac{\nabla n}{n} \rho_e - \nabla \rho_e \right) + (\Gamma - 1) \Pi_e : \nabla \left(\frac{1}{ne} \vec{J} \right) \\ + \vec{u} \cdot \nabla \rho_e + \Gamma \rho_e \nabla \cdot \vec{u} &= (\Gamma - 1) \left[Q_e - \vec{q}_e + \eta J^2 - \vec{u} \cdot \vec{F}_e - \Pi_e : \nabla u \right] \\ &+ \frac{1}{ne} \vec{J} \cdot \left(\frac{\nabla n}{n} \rho_e - \nabla \rho_e \right) + (\Gamma - 1) \left[\Pi_e : \nabla \left(\frac{1}{ne} \vec{J} \right) + \frac{1}{ne} \vec{J} \cdot \vec{E} \\ \vec{E} &= -\vec{u} \times \vec{B} + \eta \vec{J} + \frac{1}{ne} \left(\vec{J} \times \vec{B} - \nabla \rho_e - \nabla \cdot \Pi_e + \vec{F}_e \right) \\ \vec{J} &= \frac{1}{u_0} \nabla \times \vec{B} \quad , \quad \frac{\partial \vec{B}}{\partial t} = -\nabla \times \vec{E} \end{aligned}$$





 $\frac{\partial p_e}{\partial t}$





Radiated and conducted power



2 injectors

6 injectors

