

Avoidance of Neoclassical Tearing Mode Locking and Disruption by Feedback-driven Mode Rotation Control

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Theory and Simulation of Disruptions

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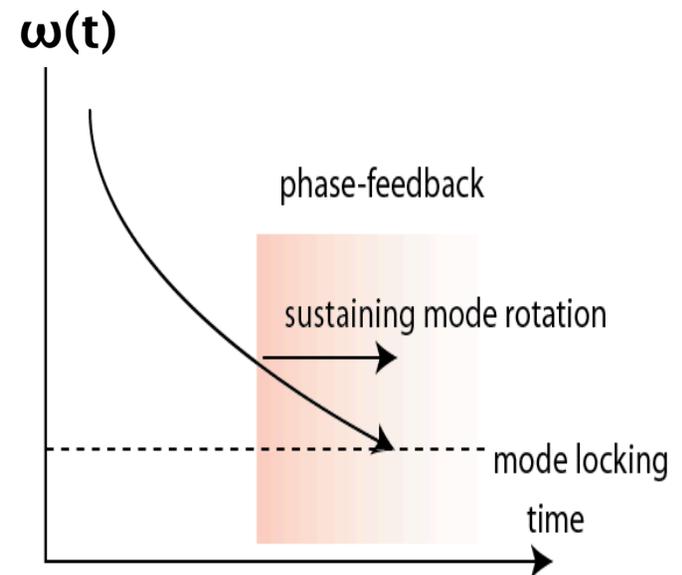
Motivation

Tokamak reactor requires:

- Assurance of NTM/TM locking avoidance is prerequisite for orderly shutdown such as the termination of hundreds Mega Joules of magnetic stored energy.

An Approach:

- Injection of the electro-magnetic (EM) torque using 3D coils by forcing finite toroidal phase shift between the mode and applied feedback field



Outline

(1) Introduction

- Two scenarios were investigated in DIII-D: preliminary results ($q_{95} \sim 4$)

(2) Sustaining high β_N NTM - Avoidance of locking and disruption

(3) Orderly shut down process by reducing NBI power

-working as Dynamic Error Field Correction as well as NTM locking avoidance

(4) A Simple Model

- Comments

(5) RFX-mod/tokamak explores independently TM-disruption avoidance with similar feedback approach → Feedback scheme seems robust

(6) ELM-like MHD bursting clouds are synchronized with NTM (possible impact on disruption process)

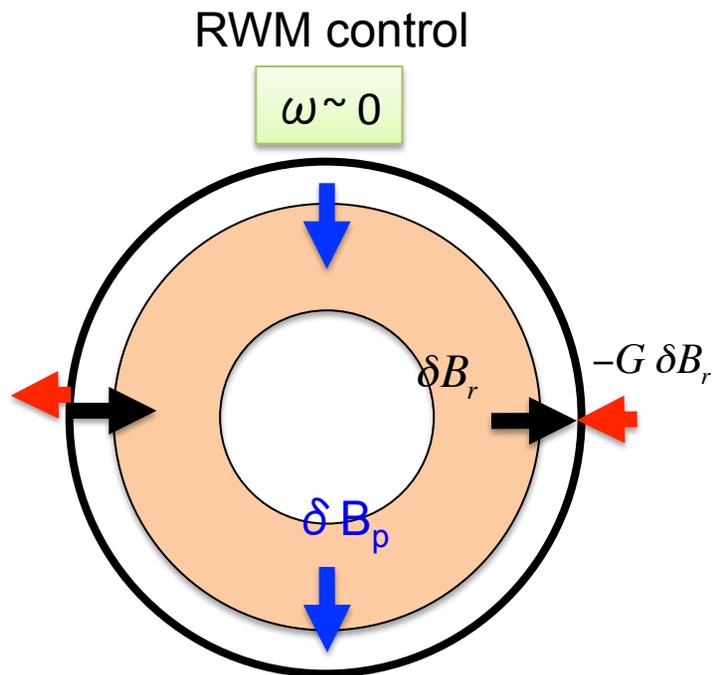
- Summary

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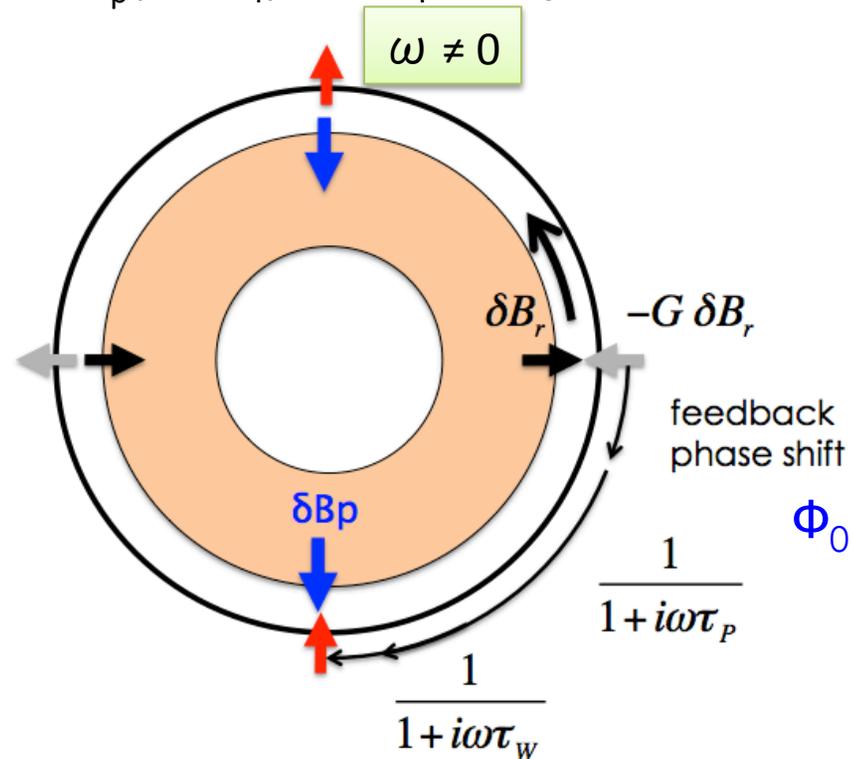
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- Two scenarios were investigated in DIII-D: preliminary results ($q_{95} \sim 4$)
 - (2) Sustaining high β_N NTM - Avoidance of locking and disruption
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 - (5) RFX-mod/tokamak explores TM-disruption with similar feedback approach
 - A reliable way for EM torque injection with 3D fields
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Feedback-driven torque control maximizes the electro-magnetic $\delta B_{p.mode} \times B_{r.ext}$ torque

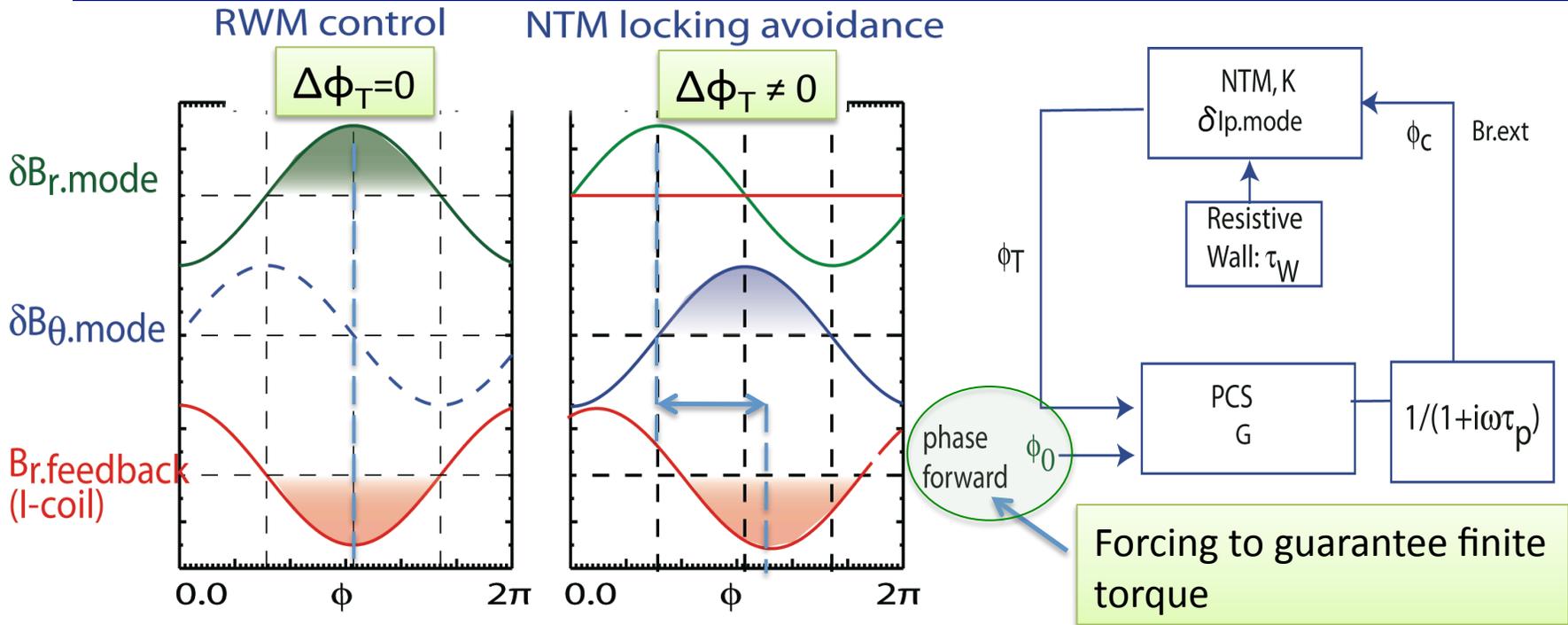


$T \propto \delta B_p (-G \delta B_r) \sin \Delta \Phi_T$: torque control



Feedback radial field phase can be synchronized with the poloidal field component of NTM by adjusting feedback parameters, such as gain G and filtering time τ_p and presetting of initial phase shift, ϕ_0

RWM control feedback functions for torque control and locking avoidance

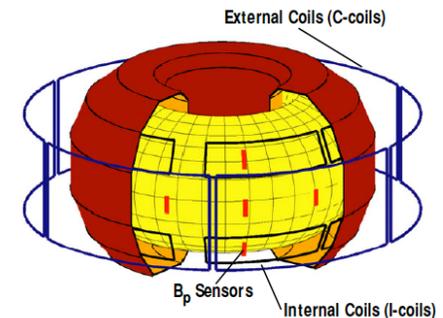


- Steady state Torque

$$\frac{\omega}{\tau_{loss}} = (Q_{NBI} / I) - (T/I) B_{r.ext} \delta B_{p.mode} \sin \Delta\phi_T$$

$$\Delta\phi_T = \angle(B_{r.ext}, \delta B_{r.modes}) = \angle(B_{r.ext}, \delta I_{p.modes}) - \pi / 2$$

Feedback_driven_mode_control



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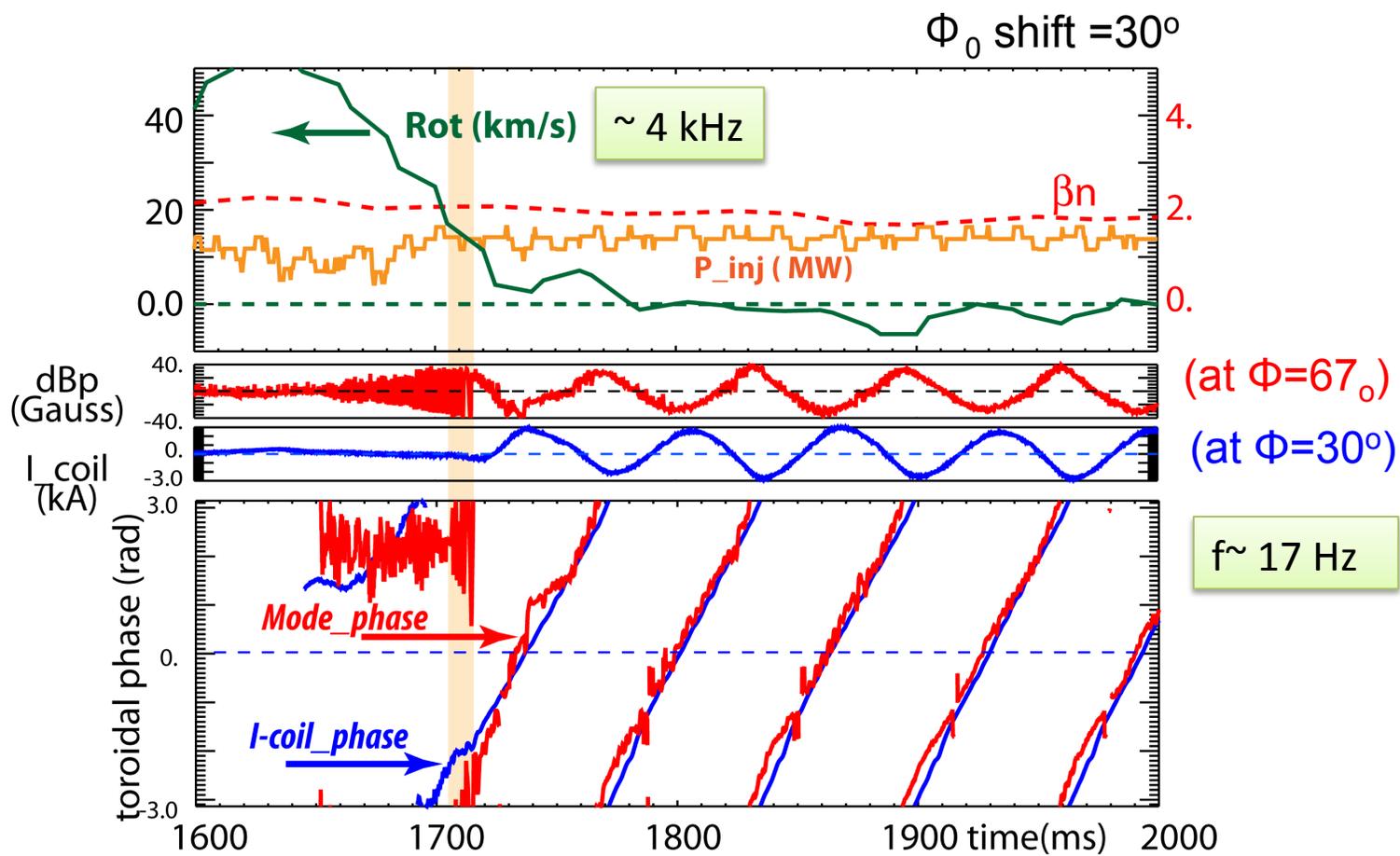
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The phases of feedback current and mode δB_p became “nearly in phase”, producing max. torque, when the mode frequency was reduced to the order of $\approx 1/\tau_p$.

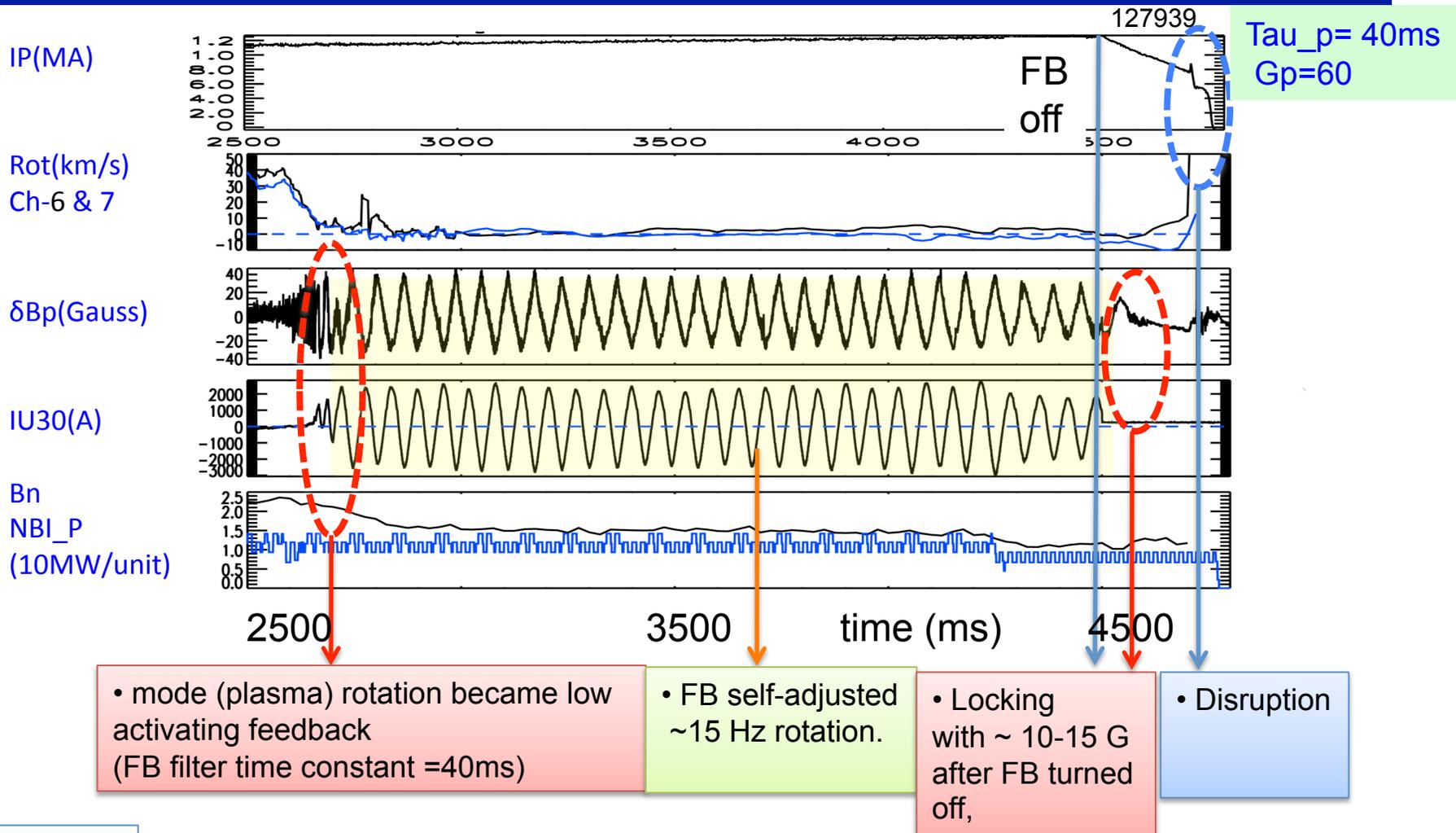


• $\tau_p=40$ ms, gain=60: typical DEFC feedback parameters ($\tau_w=2.5$ ms)

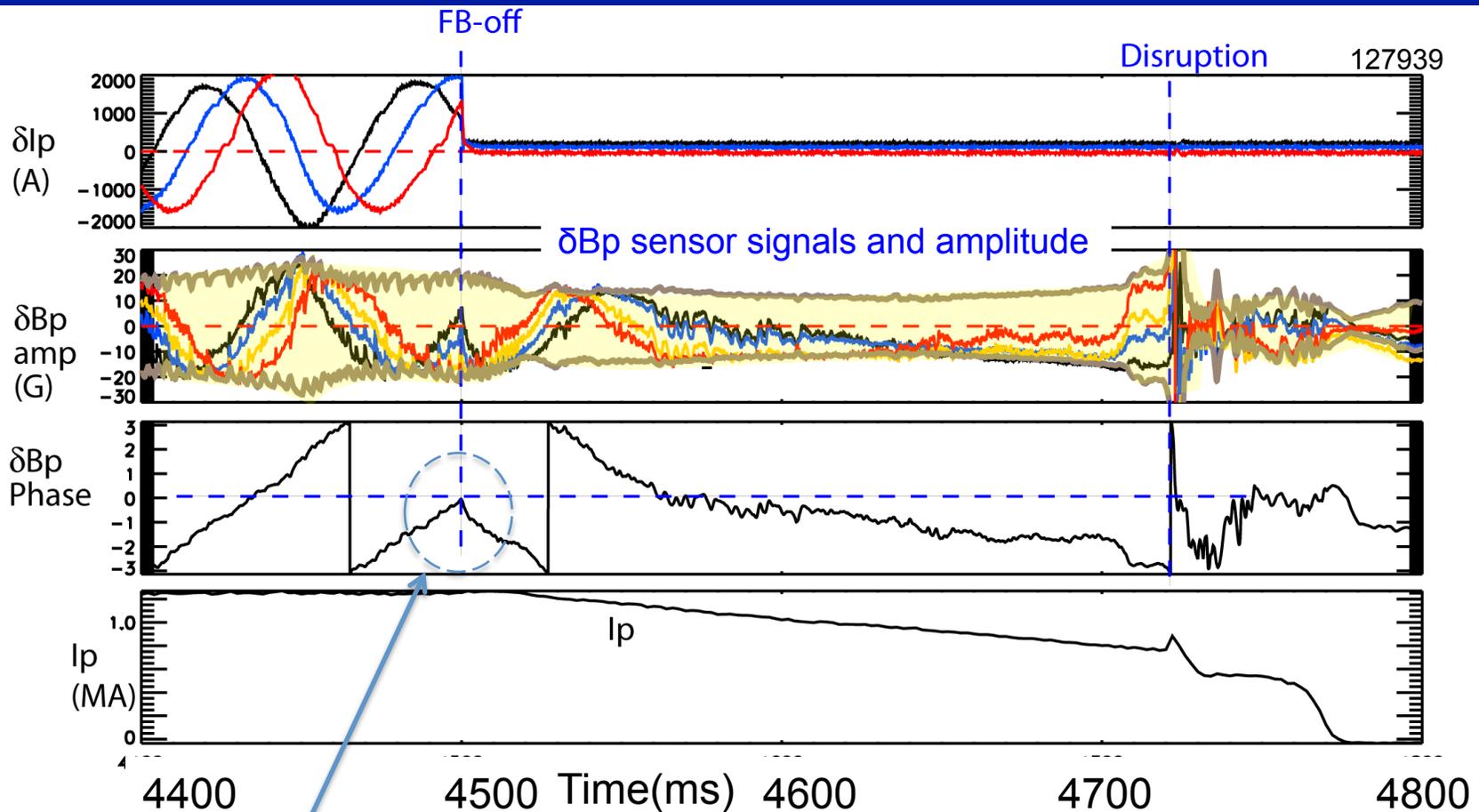
Feedback_driven_mode_control



NTM mode-locking can be avoided

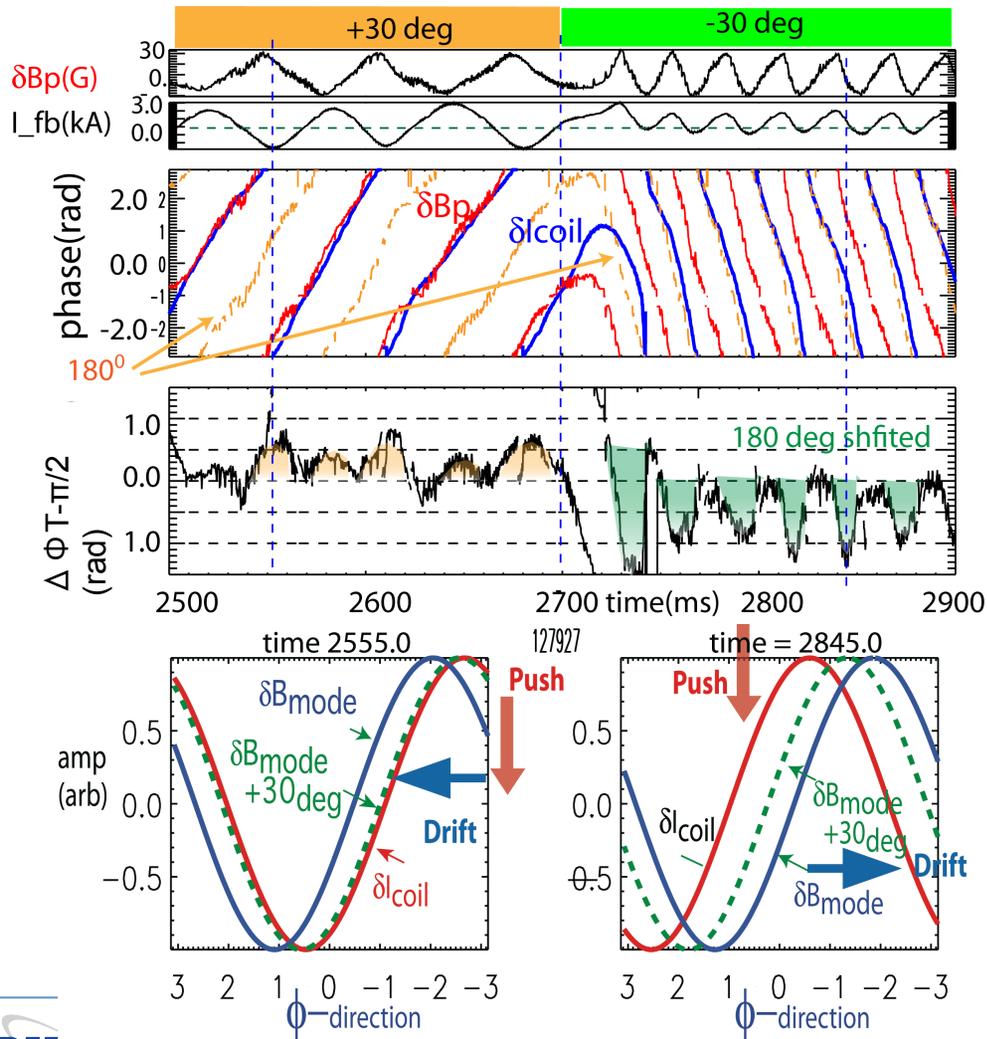


FB turning-off leads to a locked NTM and disruption



Small mode inertia

The toroidal phase offset determines the direction of mode rotation (phase shift from +30 deg \rightarrow -30 deg)



- Rotation direction changes with the 180° shift of $\delta B_{p,mode}$

- Frequency difference is due to Doppler shift by other torque

Due to forward $\delta\Phi$ shift Torque by NBI

$$f_{obs(\pm)} = \pm \delta f_{shift} + f_{doppler}$$

$$f_{obs(-)} = -14 \text{ Hz}$$

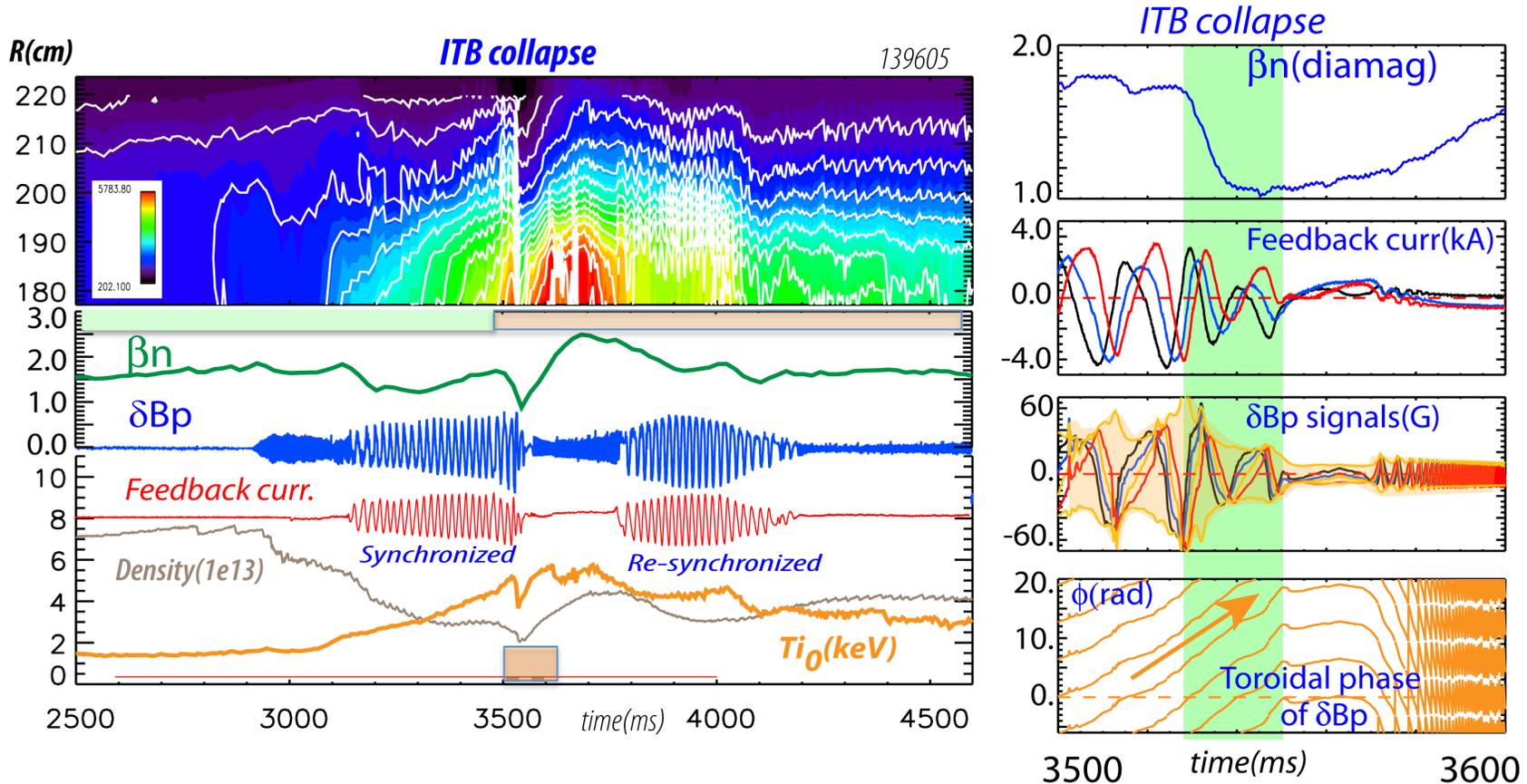
$$f_{obs(+)} = +33 \text{ Hz}$$

$$f_{doppler} = +10 \text{ Hz}$$

$$\delta f_{shift} = +24 \text{ Hz}$$



EM torque input is sufficient enough to avoid ITB collapse disruption even when the density is pumped out by NTM



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$\tau_P = 10$ ms and Gain 60



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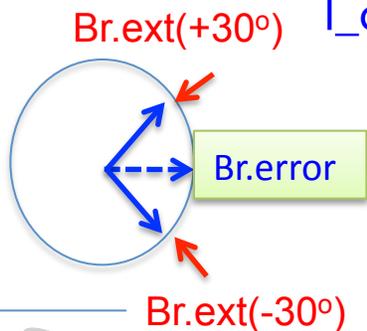
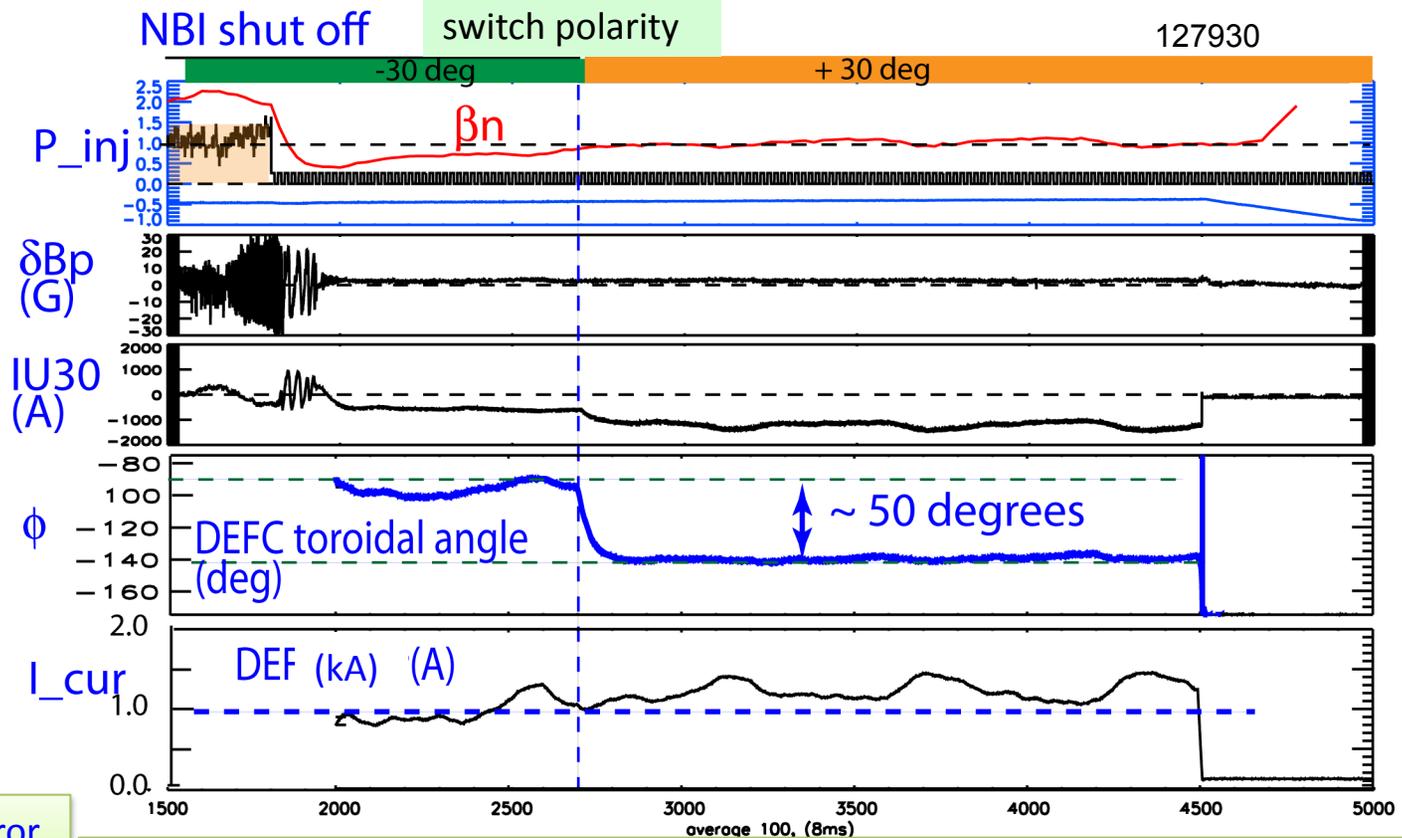
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→ A reliable way for EM torque injection with 3D fields

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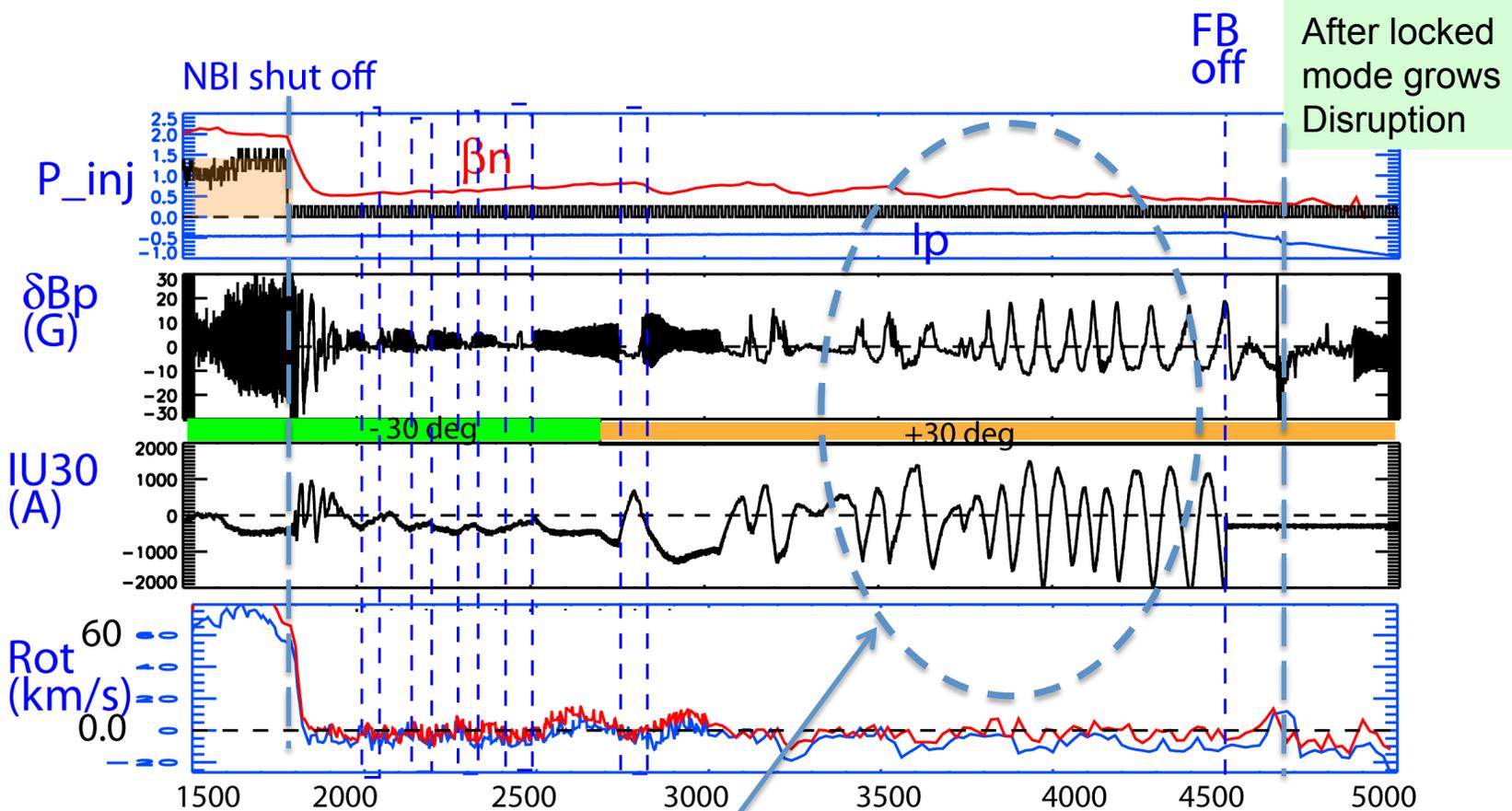
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When the NTM is suppressed, the system functions as DEFC.
 -current max. location shifts with sensor shift from +30° to -30° deg



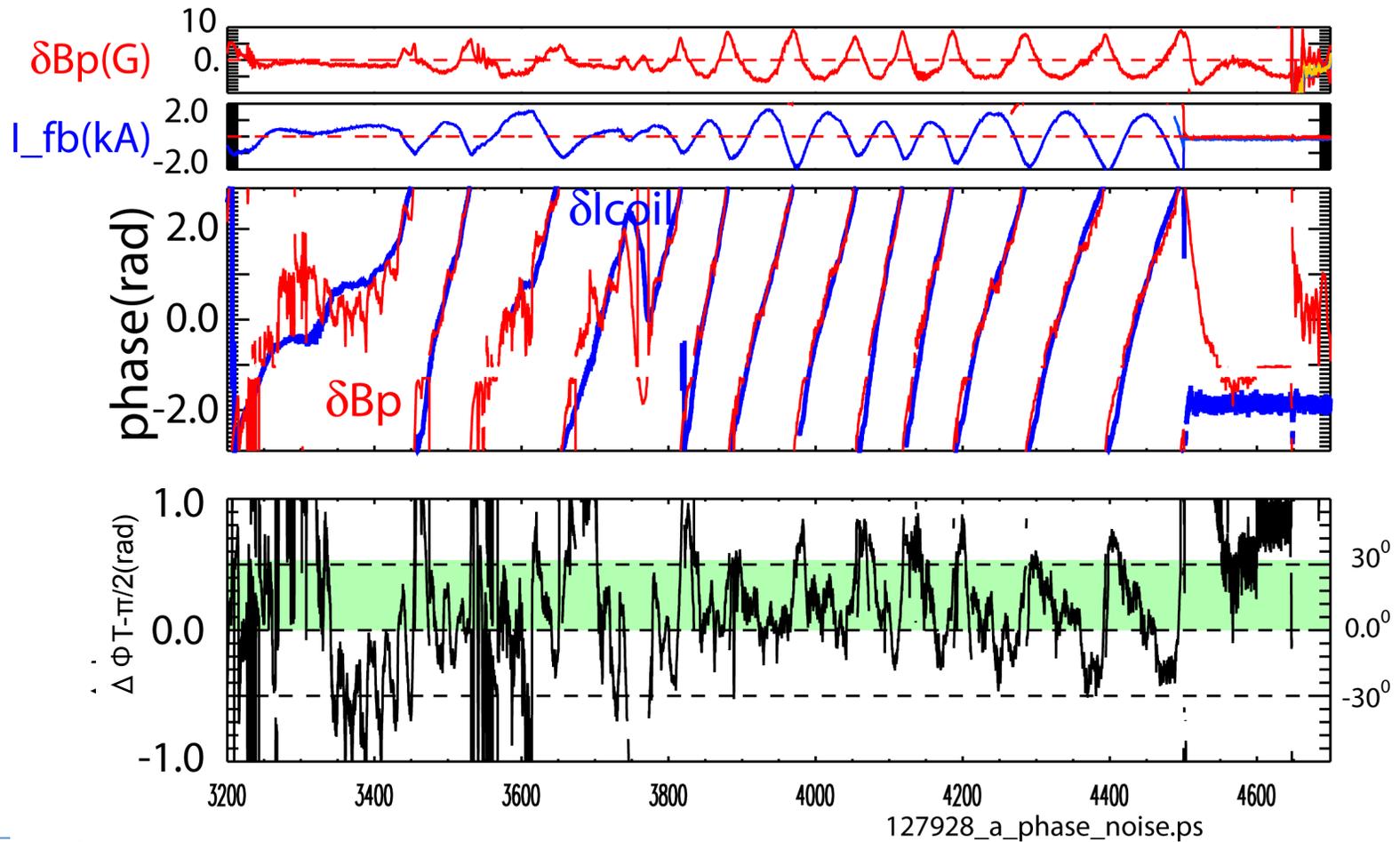
Appeared as the consequence of EFC change due to lower betan (NBI turned off)

Feedback controls the NTM/TM in an orderly shut down process

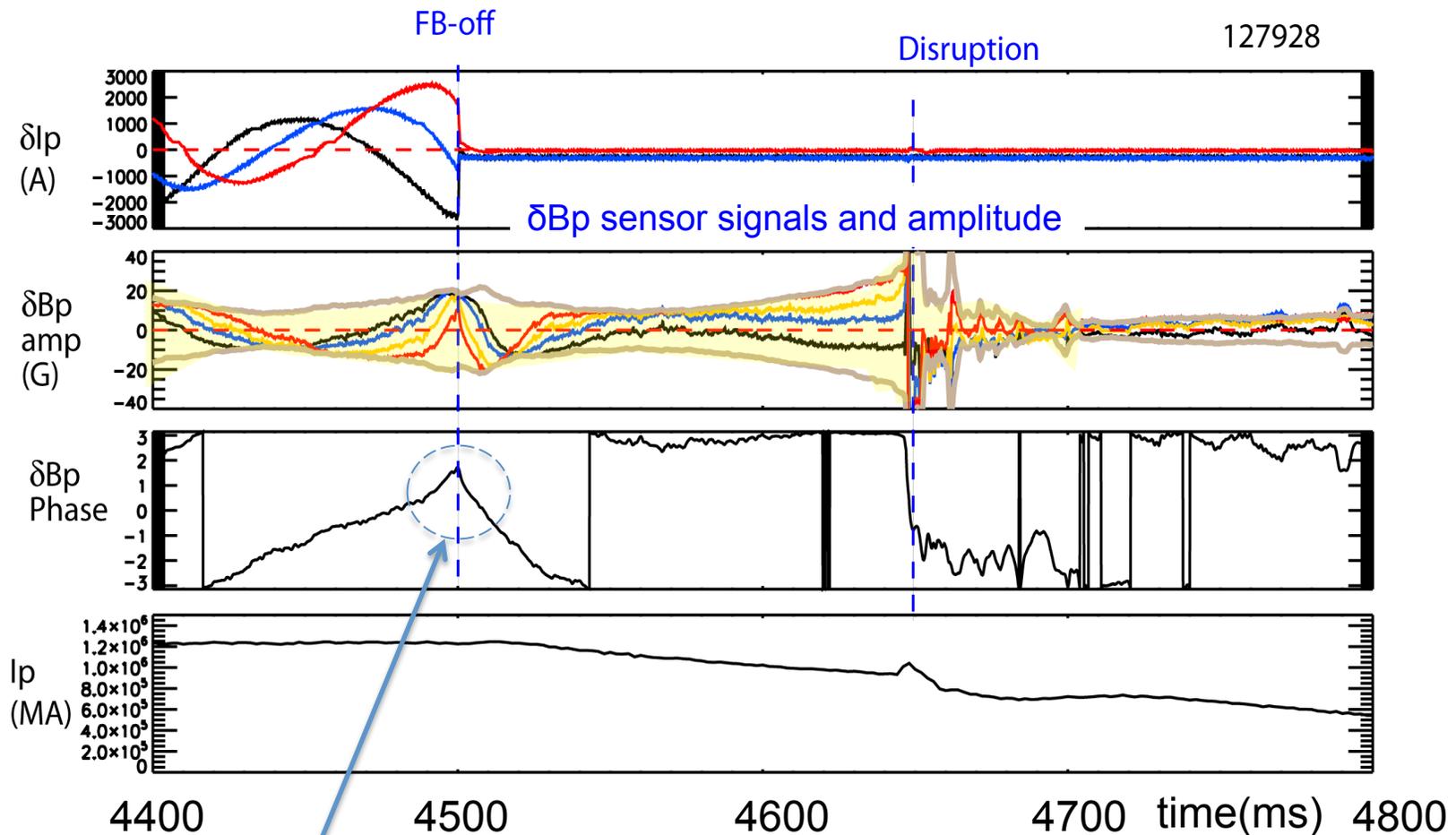


- EM torque controls the mode by self-adjusting frequency 5- 10 Hz

Maximum torque “near 90°” was provided by feedback even during lock/unlocked period

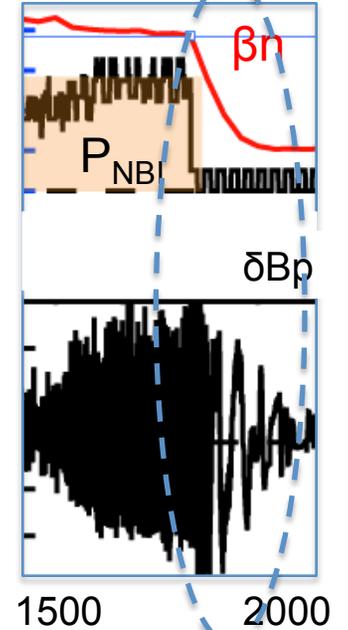
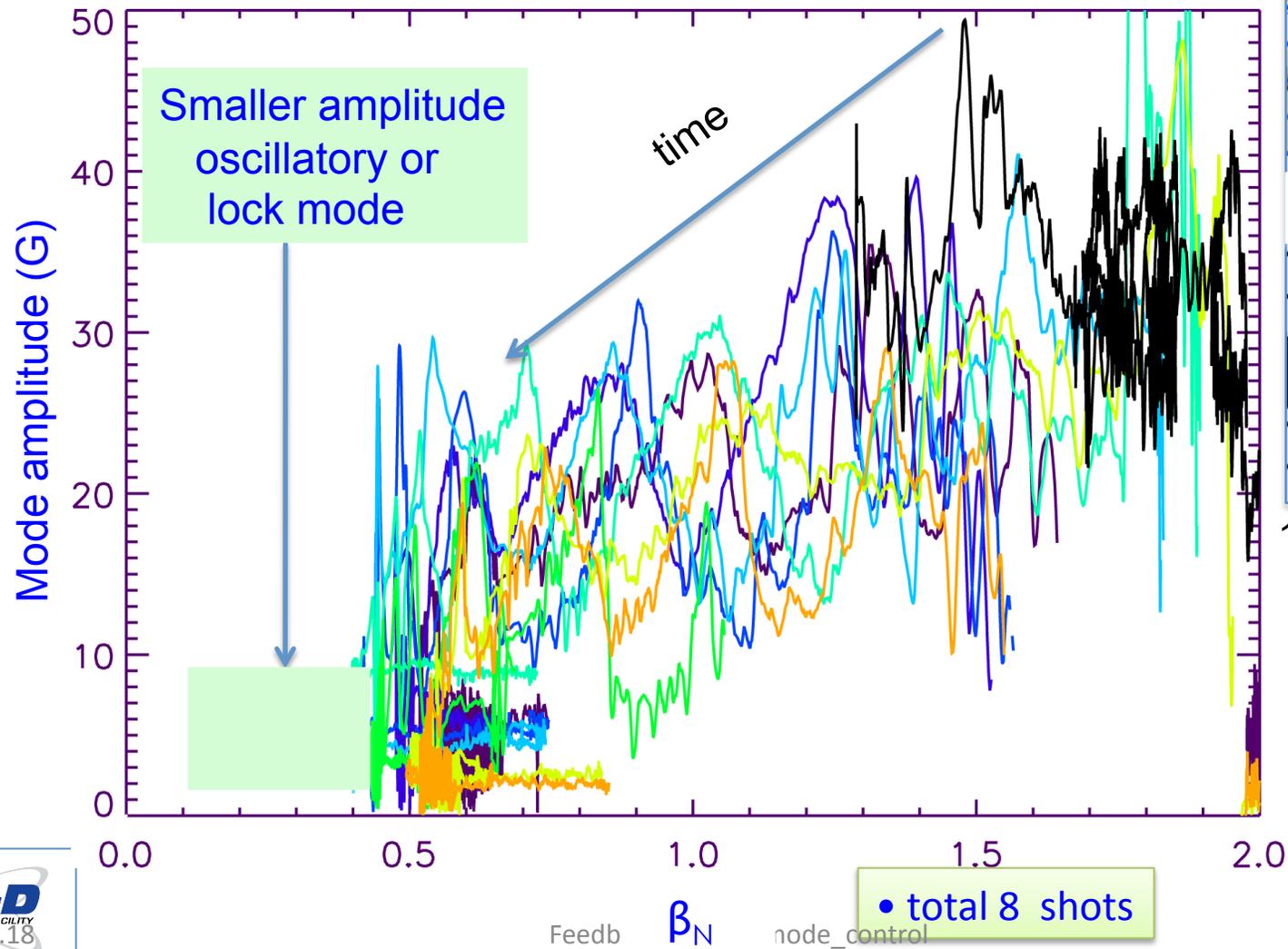


FB turning-off leads to a locked NTM and disruption



- Rapid change of direction Implies small inertia term

Feedback assisted reproducible smooth landing to lower β_N stage when NBI is terminated.



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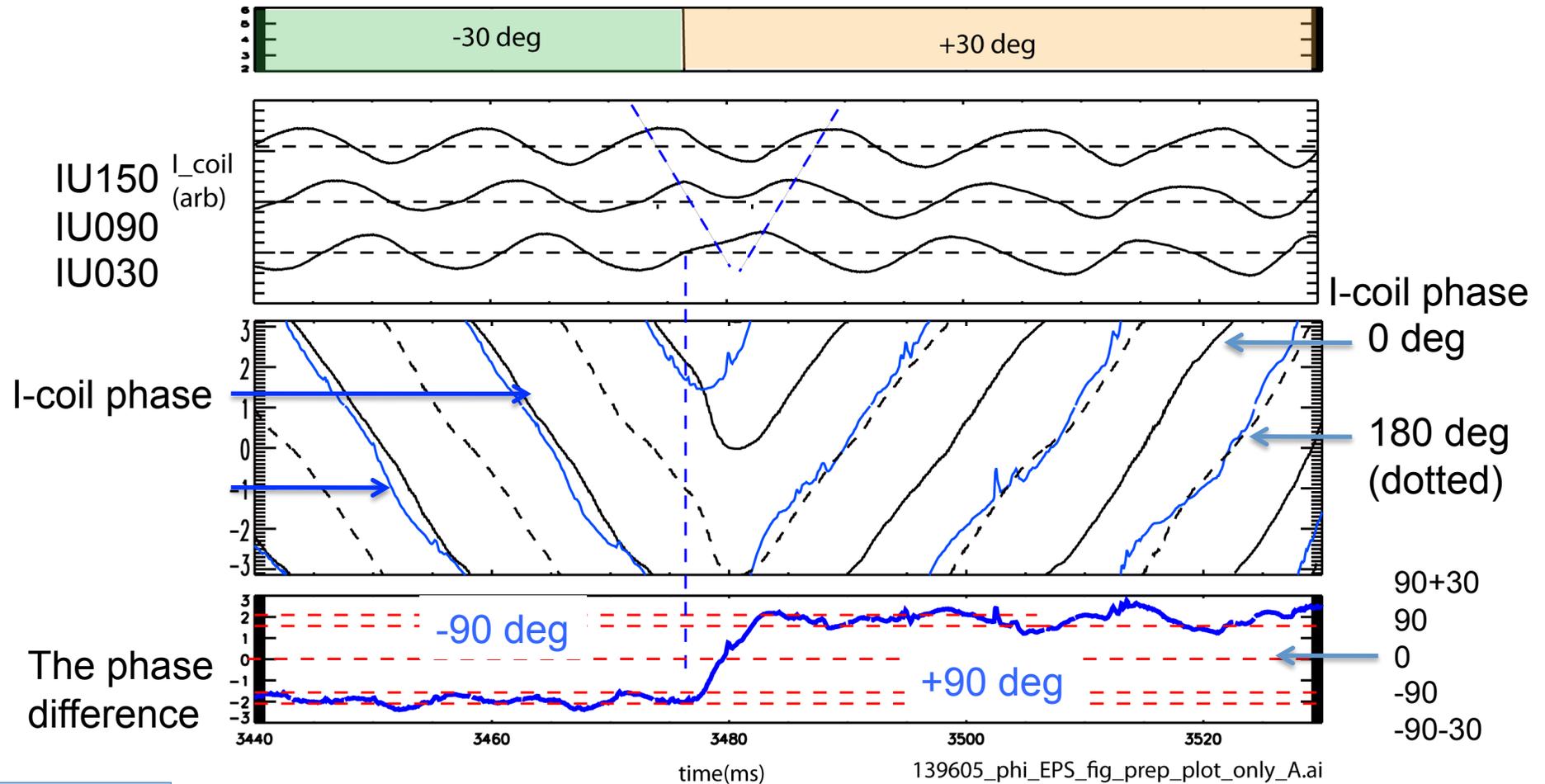
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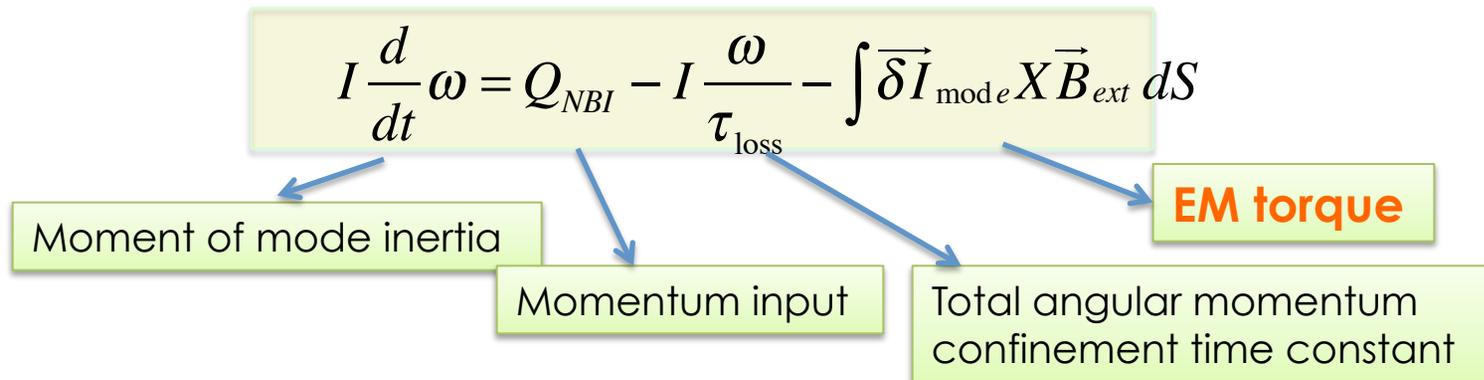
A unique feature of this approach: Presetting the phase offset leads to max. torque in the given direction



- The polarity shift causes only ~ 10 ms delay in the plasma response
 \rightarrow small mode inertia

A simple model

- Torque balance equation:



- Torque balance condition in steady state

$$\frac{\omega}{\tau_{\text{loss}}} = (Q_{NBI} / I) - (T/I) B_{r,\text{ext}} \delta B_{p,\text{mode}} \sin \Delta \phi_T$$

Here, we assume the weak loss case, $(Q_{NBI} - \omega/\tau_{\text{loss}}) \sim \text{zero limit}$

- EM torque input to NTM is dissipated by the resistive wall

A cylindrical model

Assuming the geometrical factors: the wall, sensors and coil are located close to the plasma surface

Resistive wall dissipation

Feedback field phase shift

$$\text{Torque Input: } A(\omega) = \text{Imaginary} \left\{ \left(\frac{-i\omega\tau_w}{(i\omega\tau_w + 1)} + \frac{G \exp(i\phi_0)}{(1 + i\omega\tau_w)(1 + i\omega\tau_p)} \right) |\delta B_p|^2 \right\}$$

$$\longrightarrow A(\omega) \propto \frac{f}{g}$$

$$f = -(\omega\tau_p)^3(\tau_w/\tau_p) - (\omega\tau_p)(\tau_w/\tau_p) + G \sin(\phi_0)(1 - (\omega\tau_p)^2(\tau_w/\tau_p)) - G \cos(\phi_0)(\omega\tau_p)(1 + (\tau_w/\tau_p))$$

$$g = (1 + (\omega\tau_p)^2)(1 + (\omega\tau_p)^2(\tau_w/\tau_p)^2)$$

The toroidal shift ϕ_0 preset determines the direction of mode rotation

$$A(\omega) \propto \frac{f}{g}$$

$$f = -(\omega\tau_p)^3(\tau_w/\tau_p) - (\omega\tau_p)(\tau_w/\tau_p) + G\sin(\phi_0)(1 - (\omega\tau_p)^2(\tau_w/\tau_p)) - G\cos(\phi_0)(\omega\tau_p)(1 + (\tau_w/\tau_p))$$

$$g = (1 + (\omega\tau_p)^2)(1 + (\omega\tau_p)^2(\tau_w/\tau_p)^2)$$

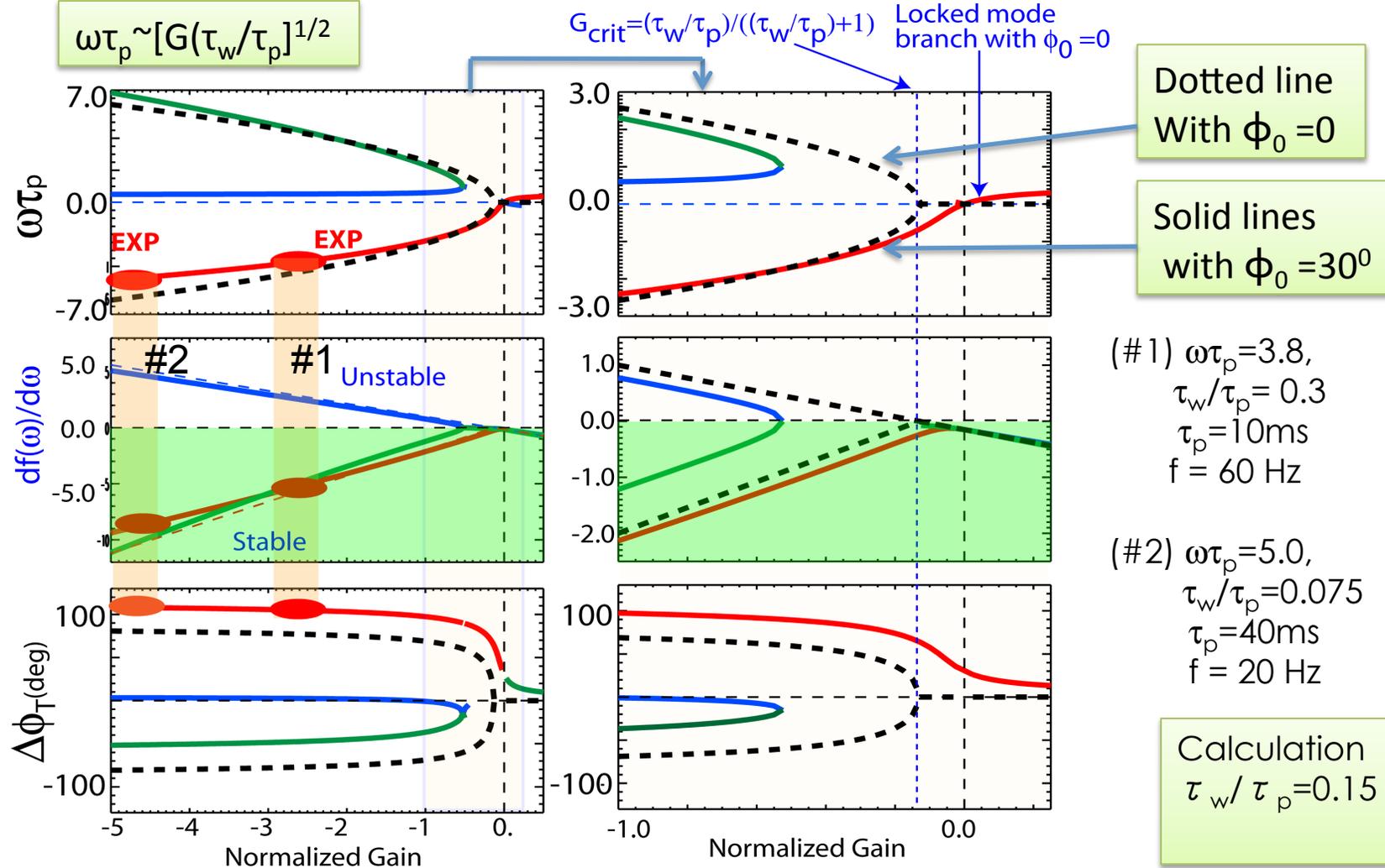
with $\omega \rightarrow -\omega$ together with $\phi_0 \rightarrow -\phi_0$

- Torque balance: $f(\omega) = 0$
- Stability of the torque balance: $\partial A/\partial\omega < 0 \rightarrow \partial f/\partial\omega < 0$

Both remain intact

\rightarrow toroidal shift ϕ_0 preset determines the mode direction.

The model predictions are consistent with key experimental observations



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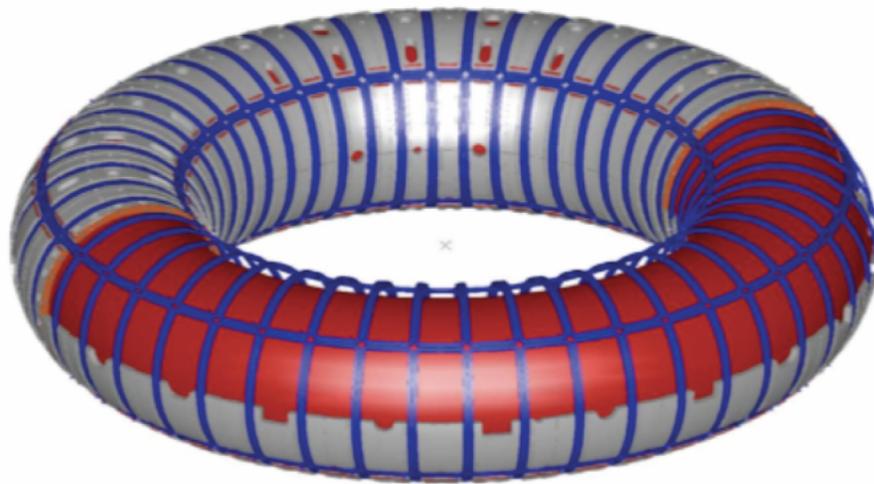
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➔ Feedback approach seems robust for EM torque injection

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RFX-Mod-tokamak also successfully avoided TM-locking and disruption by feedback-driven EM torque control
- The feedback approach seems robust--



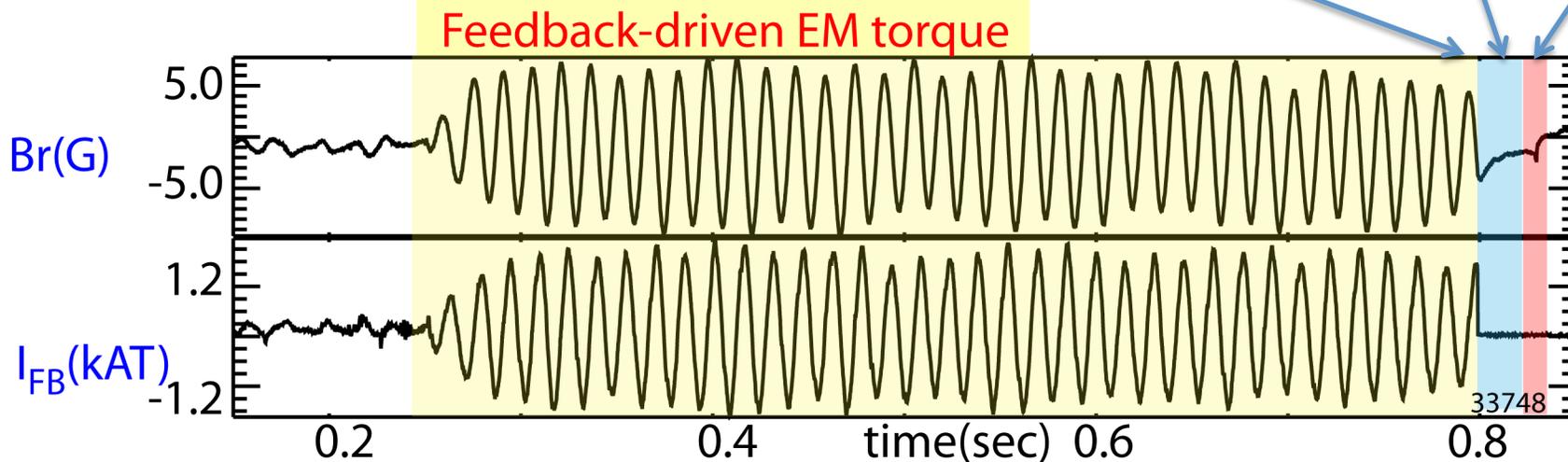
RFX-mod/Tokamak

- circular plasma
- Feedback coils outside shell:192
- shell time constant ~ 50 ms
- $q_{95} \sim 2.2$
- $n_e \sim 0.5 \times \text{GW density limit}$

Feedback turned off

Mode-locking

Disruption



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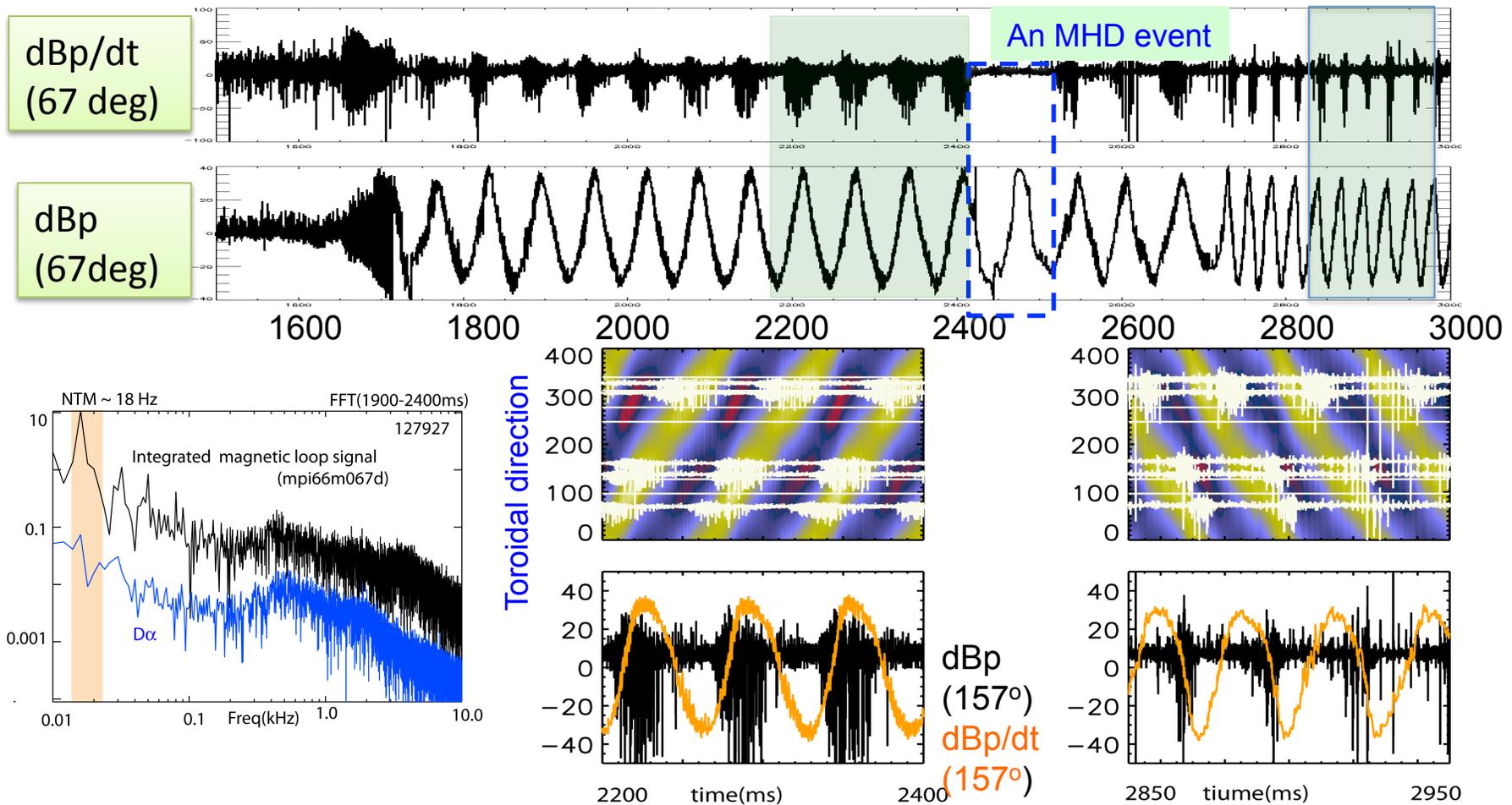
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Fast MHD bursts are located on one side of propagating slope of 18 Hz NTM



The bursting MHD behavior is similar to the ideal mode excited by the increased pressure gradient as observed in TFTR

PRL 1995, Vol 75, p1765 by W. Park, E. Fredrickson et al.: ballooning mode excited by internal kink

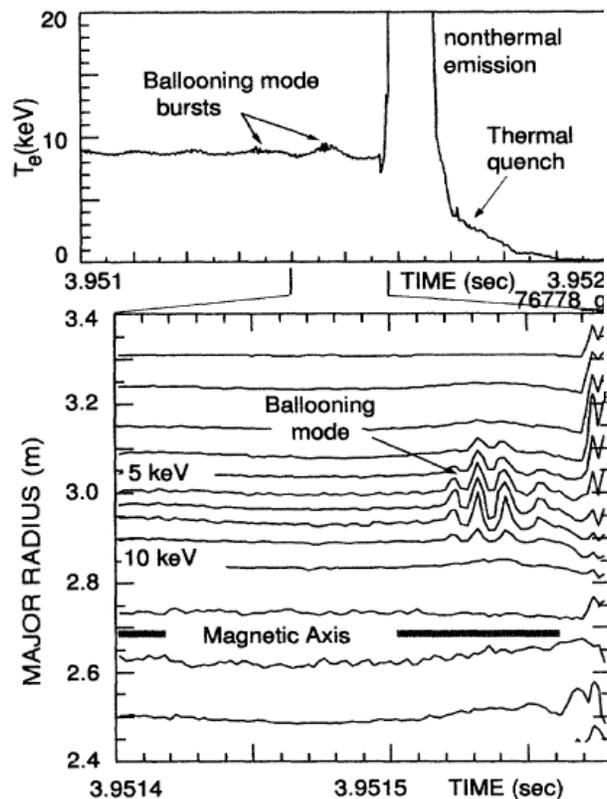
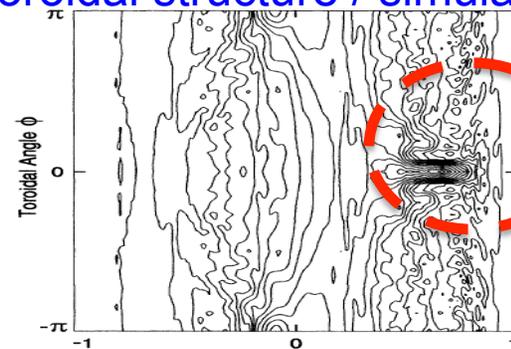


FIG. 7. The experimental ECE signals.

Toroidal structure / simulation



Extremely localized

Poloidal structure / simulation

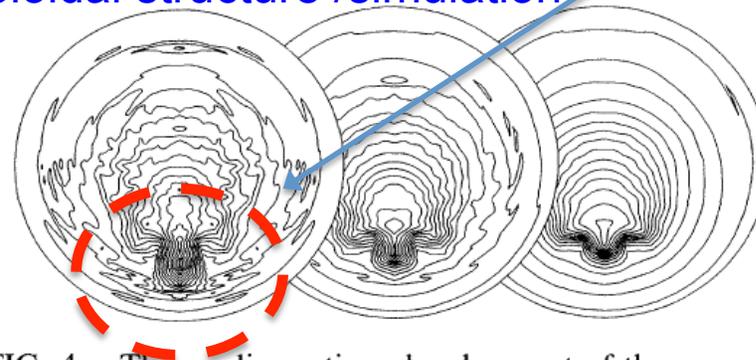


FIG. 4. The nonlinear time development of the pressure.

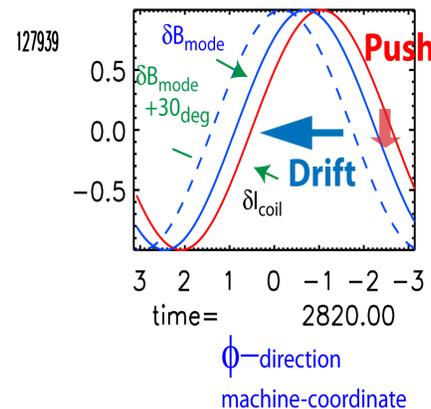
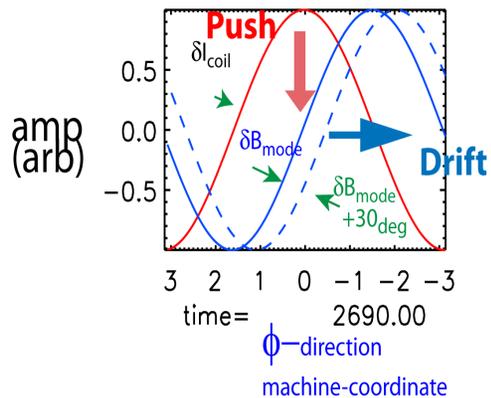
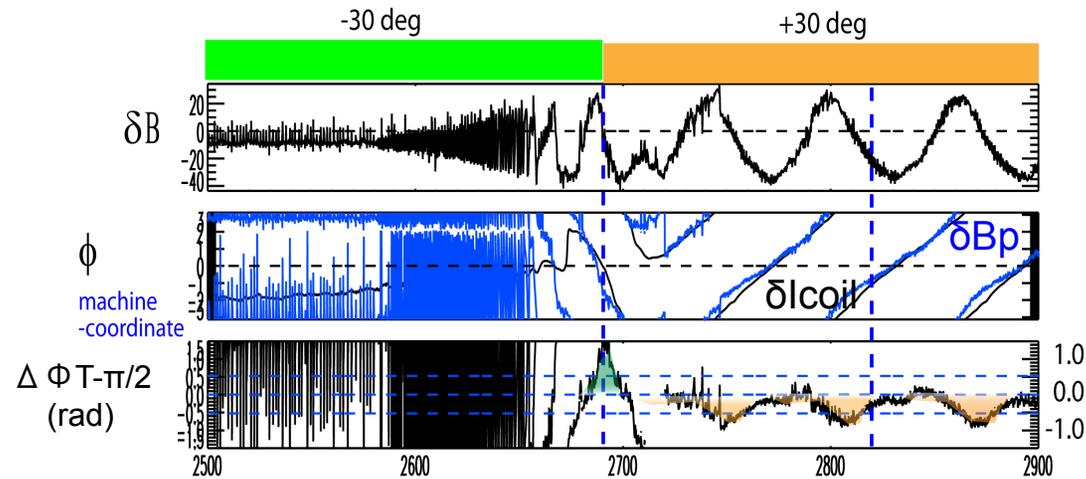
Summary

- NTM-locking disruption avoidance by **feedback-driven mode control** has been developed in DIII-D.
 - proof of principle: demonstration with two β_N levels
(so far with $q_{95} \geq 4$)
 - key elements: **forced toroidal shift, built-in DEFC**
- **Independent achievement by RFX-mod / Tokamak** implies the feedback-based EM control is **robust**.
- This feedback-based EM control scheme is useful, for example,
 - to provide orderly shutdown of magnetic energy
 - to avoid the frequency range of mechanical resonances
- Theoretical analysis of **ELM-like MHD synchronized with NTM** is important to understand NTM-locking and its disruptions

supplement



The reversed order of preset Φ^0 shows similar intrinsic rotation (preset toroidal shift from -30 deg \rightarrow +30 deg)



- A possibility of frequency change is due to Doppler shift

$$f_{\text{obs}(\pm)} = \pm \delta f_{\text{shift}} + f_{\text{doppler}}$$

$$f_{\text{obs}(-)} = -16\text{Hz}$$

$$f_{\text{obs}(+)} = +30\text{ Hz}$$

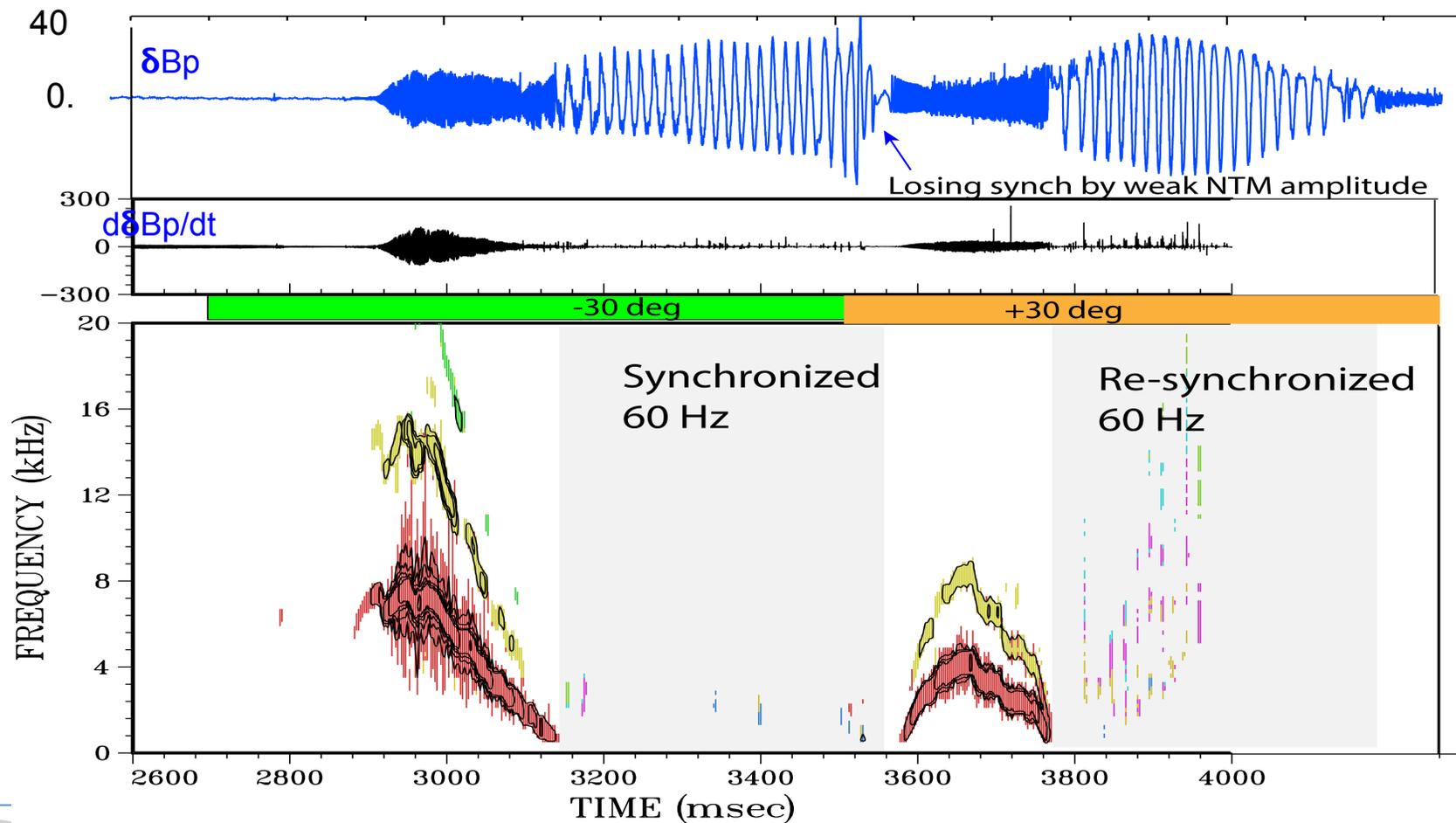
$$f_{\text{doppler}} = +7\text{ Hz}$$

$$f_{\text{shift}} = 23\text{ Hz}$$

Comparison of model and experiments

- Predictions with a simple model are consistent with various observations
 - asymptotic rotation $\omega\tau_p \sim [G(\tau_w/\tau_p)]^{1/2}$, less sensitive to details feedback settings)
- Presetting phase shift, Φ_0 improves:
 - separate **degenerated branches** near ω zero and decoupling from other modes, enhancing the stability of branches,

After the NTM is desynchronized, it can be re-synchronized when the amplitude grows



Accelerating torque sustains high β_N discharge even with a large global MHD event

