Vertical Forces during VDEs in an ITER plasma and the Role of Halo Currents

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Motivation

- Vertical Displacement Events (VDEs) are major disruption events, produced when the vertical stability control is lost.
- These events cause large currents to flow in the vessel and other adjacent metallic structures.
- These currents are due to both magnetic induction and poloidal halo current flow between the plasma and the vessel.
- The forces produced by these currents can potentially damage vessel structures and other adjacent metallic structures.
- Halo currents and their associated forces are expected to play an important role in ITER.
- Therefore, a better understanding of these halo currents and their associated forces is needed.

In this work...

- We used the M3D-C¹ code to simulate VDEs in an ITER plasma with special attention to the role of halo currents and the forces produced by them.
- We covered a wide range of cases, from small to large halo currents to look for the worst case scenario that could plausibly occur.
- We will show that both inductive and halo forces are related and, for similar conditions, changing the halo currents does not change the total vertical force since it is offset by the toroidal contribution.
- We have used the 2D version of the code (axisymmetric). A 2D benchmark was recently done. 3D simulations are underway.

2D non-linear VDEs in an ITER plasma

- Based on standard 5.3 T 15 MA ITER scenario.
- Used realistic parameters for wall resistivity. It was adjusted to give the correct $\tau = L/R$ time (235 ms).
- Started from equilibrium and perturbated it to produce the VDE instability.
- When $q_{sep} \approx 2$ the thermal quench is initiated by increasing the plasma thermal conductivity κ_{\perp} :

$$\frac{3}{2}n\frac{\partial T}{\partial t} = -\nabla \cdot \boldsymbol{q} + \eta \mathbf{J}^2 + (\dots)$$
$$\boldsymbol{q} = \kappa_{\perp} \nabla_{\perp} T + \kappa_{\parallel} \nabla_{\parallel} T$$

A general picture...

Screenshots of a VDE



A general picture...

Some global quantities vs. time



Vertical force and halo currents

$$\hat{z} \cdot \mathbf{F}_{V} = \hat{z} \cdot \int_{vessel} \mathbf{J} \times \mathbf{B} \, \mathrm{d}V = \int_{vessel} \left(-J_{\varphi}B_{R} + J_{R}B_{\varphi}\right) \mathrm{d}V$$

The $J_{\varphi}B_R \rightarrow$ due to toroidal induction. The $J_R B_{\varphi} \rightarrow$ due to halo currents.

Can we increase the halo current in order to increase the total vertical force?

In 2D simulation we initiate the TQ by increasing the thermal conductivity κ_{\perp} . We can do it in different ways:

- Varying the thermal conductivity magnitude and profile.
- Varying the temperature at the boundary.

We generated a series of cases with different halo currents to analyze their effects.

Basically, in the open field line (halo) region:

higher temperature \rightarrow lower plasma resistivity \rightarrow higher currents.

I. Uniform post-TQ κ_{\perp}

Dependance of post-TQ temperature on κ_{\perp} values



- Smaller κ_{\perp} values \rightarrow higher post-TQ T_e .
- Halo region is naturally formed after the TQ.
- Changing κ in this way has only small effect on open-field-line temperature.

I. Uniform post-TQ κ_{\perp}

Effect of varying κ on global plasma parameters



- Smaller κ_{\perp} values \rightarrow higher post-TQ $T_e \rightarrow$ slower CQ.
- Slower CQ \rightarrow slower upward motion.
- Larger vertical forces for high T_e .
- Only small dependence of maximum halo current magnitude on κ (< 1 MA)

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- Slower CQ \rightarrow slower upward motion.
- Larger vertical forces for high T_e .
- Only small dependence of maximum halo current magnitude on κ (< 1 MA)
- We select the case $T_e \sim 30$ eV as a reference

Effect of varying κ profiles on post-TQ T_e and halo current.



- Compare κ constant, increasing, or decreasing in radius
- κ decreasing in radius leads to largest T_e on open field lines \rightarrow halo current

Effect of varying κ profiles on post-TQ T_e and halo current



- Compare κ constant, increasing, or decreasing in radius
- κ decreasing in radius leads to largest T_e on open field lines \rightarrow halo current
- To increase even more the halo current, we increased the boundary temperature from 0.17 eV to 3 eV.

Effect of varying κ profiles on global plasma parameters



- κ decreasing with radius leads to slower CQ and larger halo current.
- **Increasing** boundary T_e strength these effects.
- Total vertical force largely unaffected.

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Comparison and breakdown of forces



- Larger halo current had larger $J_r B_{\phi}$ term, as expected,
- but, it is offset by a stronger reduction in the $J_{\phi}B_{r}$ contribution.
- Total vertical force is almost unaffected by magnitude of halo current.

Comparison and breakdown of forces

Relationship between inductive toroidal and poloidal halo wall forces

It is possible to write the total force on the vessel as (*)

$$F_{v} = F_{v}^{tor} + F_{v}^{pol} = -F_{c}$$

The halo formation after the TQ occurs in a timescale ($\tau \leq 10$ ms) much shorter than the dissipation time of wall currents (L/R = 235 ms). Thus, the vessel "acts" as an almost perfect conductor during this process.

Therefore, the poloidal flux outside the vessel does not change implying that F_c and, as a consequence F_v , remains constant.

Comparison and breakdown of forces

How toroidal contribution offsets the poloidal halo force?



The halo region formation produces a current density centroid displacement



Summary

We performed a series of 2D-VDE simulations varying

- the post-TQ thermal conductivity and
- the post-TQ temperature boundary condition

in order to cover a wide range of cases.

- We found that vertical wall force shows a dependence on post-TQ temperature.
- Slower CQ generally lead to larger vertical forces:
 - for CQ times short compared to vessel L/R time.
 - However, the presence of halo currents can modify this scaling.
- We showed that vertical wall force shows a very weak dependence on halo current magnitude.
 - Toroidal contribution to the total force compensates the halo contribution.

Moving forward...

- We have already started 3D non-linear simulations.
 - kink instabilities and sideways force.
- Implementing a more realistic wall with anisotropic wall resistivity.
- Working in coupling M3D-C¹ results with the CARRIDI engineering code (actual vessel).

Extra slides...

Poloidal unstructured mesh



3D Extended MHD Equation in M3D-C¹

$$\begin{aligned} \frac{\partial n}{\partial t} + \nabla \bullet (n\mathbf{V}) &= \nabla \bullet D_n \nabla n + S_n \\ \frac{\partial \mathbf{A}}{\partial t} &= -\mathbf{E} - \nabla \Phi, \quad \mathbf{B} = \nabla \times \mathbf{A}, \quad \mathbf{J} = \nabla \times \mathbf{B}, \quad \nabla_{\perp} \bullet \frac{1}{R^2} \nabla \Phi = -\nabla_{\perp} \bullet \frac{1}{R^2} \mathbf{E} \\ nM_i (\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \bullet \nabla \mathbf{V}) + \nabla p &= \mathbf{J} \times \mathbf{B} - \nabla \bullet \mathbf{\Pi}_i + \mathbf{S}_m \end{aligned}$$

$$\mathbf{E} + \mathbf{V} \times \mathbf{B} = \frac{1}{ne} (\mathbf{R}_e + \mathbf{J} \times \mathbf{B} - \nabla p_e - \nabla \bullet \mathbf{\Pi}_e) - \frac{m_e}{e} \left(\frac{\partial \mathbf{V}_e}{\partial t} + \mathbf{V}_e \bullet \nabla \mathbf{V}_e \right) + \mathbf{S}_{CD} \\ \frac{3}{2} \left[\frac{\partial p_e}{\partial t} + \nabla \bullet (p_e \mathbf{V}) \right] = -p_e \nabla \bullet \mathbf{V} + \frac{\mathbf{J}}{ne} \bullet \left[\frac{3}{2} \nabla p_e - \frac{5}{2} \frac{p_e}{n} \nabla n + \mathbf{R}_e \right] + \nabla \left(\frac{\mathbf{J}}{ne} \right) : \mathbf{\Pi}_e - \nabla \bullet \mathbf{q}_e + Q_\Delta + S_{eE} \\ \frac{3}{2} \left[\frac{\partial p_i}{\partial t} + \nabla \bullet (p_i \mathbf{V}) \right] = -p_i \nabla \bullet \mathbf{V} - \mathbf{\Pi}_i : \nabla \mathbf{V} - \nabla \bullet \mathbf{q}_i - Q_\Delta + S_{iE} \\ \mathbf{R}_e = \eta ne \mathbf{J}, \quad \mathbf{\Pi}_i = -\mu \left[\nabla \mathbf{V} + \nabla \mathbf{V}^{\dagger} \right] - 2(\mu_e - \mu) (\nabla \bullet \mathbf{V}) \mathbf{I} + \mathbf{\Pi}_i^{GV} \\ \mathbf{q}_{e,i} = -\kappa_{e,i} \nabla T_{e,i} - \kappa_{\parallel} \nabla_{\parallel} T_{e,i} \\ \mathbf{\Pi}_e = (\mathbf{B} / B^2) \nabla \bullet \left[\lambda_h \nabla \left(\mathbf{J} \bullet \mathbf{B} / B^2 \right) \right], \quad Q_\Delta = 3m_e(p_i - p_e) / (M_i \tau_e) \end{aligned}$$

Blue terms are 2-fluid terms. NOT reduced MHD.

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Using the appropriate L/R time

- Applied a constant loop voltage at the domain boundary.
- Without any plasma, the system behaves as a basic LR-circuit.

$$I(t) = \begin{cases} I_0 \left(1 - e^{-t/\tau} \right) \\ I_c e^{-(t - t_c)/\tau} \end{cases}$$



$\kappa_{\parallel}/\kappa_{\perp}$ effect on the open field line T_e

• Inside the plasma: the post-TQ temperature profile is mostly determined by κ_{\perp}

 $T_{TQ} \approx \kappa_{\perp TQ}^{-2/5}$

• Outside the plasma: κ_{\parallel} links the plasma temperature with the boundary condition. Assuming $T_{SOL} \sim e^{-\alpha x}$, very simplified $\alpha \sim \alpha(\sqrt{\kappa_{\parallel}/\kappa_{\perp}})$ dependence can be derived.



Poloidal halo currents patterns for both cases



Poloidal halo currents can follow different paths and generate a complex pattern.

Current breakdown



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